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**THE EFFECTIVENESS OF EMG-DRIVEN NEUROMUSCULOSKELETAL
MODEL CALIBRATION IS TASK DEPENDENT**

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ABSTRACT

Calibration of neuromusculoskeletal models using functional tasks is performed to calculate subject-specific musculotendon parameters, as well as coefficients describing the shape of muscle excitation and activation functions. The objective of the present study was to employ a neuromusculoskeletal model of the shoulder driven entirely from muscle electromyography (EMG) to quantify the influence of different model calibration strategies on muscle and joint force predictions. Three healthy adults performed dynamic shoulder abduction and flexion, followed by calibration tasks that included reaching, head touching as well as active and passive abduction, flexion and axial rotation, and submaximal isometric abduction, flexion and axial rotation contractions. EMG data were simultaneously measured from 16 shoulder muscles using surface and intramuscular electrodes, and joint motion evaluated using video motion analysis. Muscle and joint forces were calculated using subject-specific EMG-driven neuromusculoskeletal models that were uncalibrated and calibrated using (i) all calibration tasks (ii) sagittal plane calibration tasks (iii) scapular plane calibration tasks. Joint forces were compared to published instrumented implant data. Calibrating models across all tasks resulted in glenohumeral joint force magnitudes that were more similar to instrumented implant data than those derived from any other model calibration strategy. Muscles that generated greater torque were more sensitive to calibration than those that contributed less. This study demonstrates that extensive model calibration over a broad range of contrasting tasks produces the most accurate and physiologically relevant musculotendon and EMG-to-activation parameters. This study will assist in development and deployment of subject-specific neuromusculoskeletal models.

INTRODUCTION

The evaluation of musculotendon parameters, as well as coefficients describing the shape of the muscle excitation and activation functions, presents a challenge in EMG-driven neuromusculoskeletal modelling. These values must be estimated using a calibration process that matches model estimates of net joint moments to those calculated directly from inverse dynamics over a specific set of tasks. At the shoulder, musculotendon calibration has been achieved using isometric contractions and dynamic joint motion including activities of daily living (Kian et al., 2019, Assila et al., 2020). However, the dependence of the chosen calibration tasks on neuromusculoskeletal model estimates of muscle and joint loading remain poorly understood, and the chosen calibration tasks are known to be a significant source of model output variability. The aim of this study was to employ an EMG-driven neuromusculoskeletal model of the shoulder to quantify the influence of model calibration tasks on muscle and joint force predictions. The findings will have implications for development and deployment of EMG-driven and EMG-informed neuromusculoskeletal models.

MATERIALS AND METHODS

Subject recruitment and testing

Three healthy female adults with no history of upper limb pain, disease or previous surgery were recruited for testing (mean age: 23.7 ± 6.4 years; body mass: 55.7 ± 3.2 kg; height: 165.0 ± 2.6 cm). Testing followed a previously published protocol and is only briefly described here (Kian et al., 2019). The participants performed dynamic shoulder movements while standing which included shoulder abduction and flexion at a rate of 60° per second. The participants then performed three sets of calibration tasks comprising general movements, and sagittal plane and scapular plane tasks, which were chosen because they span different mechanical degrees of freedom (DOF) at the shoulder. The general calibration movements

25 were reaching, head touching and submaximal isometric internal and external rotation of the
26 shoulder with the arm in 90° of abduction and the elbow flexed to 90°, while the sagittal plane
27 tasks incorporated (i) active flexion of the shoulder at approximately 30° per second with the
28 elbow extended, (ii) passive flexion of the shoulder, and (iii) sub-maximal isometric flexion
29 and extension of the shoulder with the arm in 90° of flexion. The scapular plane tasks consisted
30 of (i) abduction at approximately 30° per second with the elbow extended, (ii) passive
31 abduction of the shoulder, and (iii) sub-maximal isometric abduction and adduction of the
32 shoulder with the arm in 90° of abduction. All isometric contractions were performed using an
33 instrumented handle and consisted of four seconds of gradual load increase to 50% maximal
34 effort, three seconds of sustained contraction at 50% maximal effort, followed by four seconds
35 of load decrease to resting level. Subjects followed a visual trajectory of their contraction on a
36 monitor to guide their contraction execution. Ethical approval was obtained through the
37 University of Sydney Human Research Ethics Committees, and participants provided written
38 informed consent.

39 During testing, pairs of surface EMG electrodes (Red Dot, 2258, 3M) were placed over
40 pectoralis major, upper trapezius, lower trapezius, biceps brachii and triceps brachii. Bipolar
41 intramuscular (in-dwelling) electrodes were placed in anterior, middle and posterior deltoid
42 sub-regions, rhomboid major, supraspinatus, infraspinatus, subscapularis, pectoralis minor,
43 serratus anterior, teres major, and latissimus dorsi (Boettcher et al., 2008, Johnson et al., 2011,
44 Ginn and Halaki, 2015), with ultrasonic guidance employed for rhomboid major and pectoralis
45 minor electrode placement (Mindray, DP-9900). Upper limb joint kinematics was
46 simultaneously recorded during testing using a 4-camera video motion analysis system (Vicon,
47 UK). The trajectories of 15 retroreflective markers placed on the upper-limb were digitised and
48 inverse kinematics employed to calculate joint angles (Wu et al., 2016).

49

50 *Musculoskeletal modelling*

51 EMG-driven neuromusculoskeletal model of each participant were created as described
52 previously (Kian et al., 2019). Each model comprised 5-segments and 10 degree-of-freedom.
53 The glenohumeral and acromioclavicular joints were modeled as 3-degree-of-freedom ball and
54 socket joints, and the sternoclavicular and elbow joints as 2-degree-of-freedom universal joints.
55 The joints were actuated by 23 Hill-type musculotendon units, which comprised 5 axiohumeral,
56 10 axioscapular and 8 scapulohumeral muscles and muscle sub-regions. Each muscle's neural
57 excitation was calculated from its pre-processed EMG signal using a second order linear
58 differential equation cast as a numerical backward differences formula:

$$u(t) = \alpha e(t - d) - (C_1 + C_2)u(t - 1) + C_1 \cdot C_2 u(t - 2) \quad \text{Equation 1}$$

59 where $e(t)$ is the time-varying muscle excitation, $u(t)$ the neural excitation, d the
60 electromechanical delay, α a muscle gain coefficient, and C_1 and C_2 recursive coefficients
61 (Lloyd and Besier, 2003). Muscle activation was modeled using a non-linear neural excitation
62 function (Lloyd and Besier, 2003):

63

$$a(t) = \frac{e^{A \cdot u(t)} - 1}{e^A - 1} \quad \text{Equation 2}$$

64 where $a(t)$ is the time-varying muscle activation, $u(t)$ the time-varying neural excitation
65 and A , a non-linear shape factor ranging between zero (a straight-line) and 3 (highly non-
66 linear). Muscle forces were subsequently calculated using a Hill-type model of each
67 musculotendon actuator:

$$F^m(t) = F^t(t) = F^{max} [f_a(l_m) \cdot f_v(v_m) \cdot a(t) + f_p(l_m) + d_m \cdot v_m] \cdot \cos \varphi \quad \text{Equation 3}$$

68 where $F^m(t)$ is the time-varying force generated by the sum of muscle fibers, F^t the
69 tendon force, F^{max} the maximum isometric muscle force, $f_a(l_m)$ the active force-length
70 relation, $f_v(v_m)$ the muscle fibre contraction velocity relation, $f_p(l_m)$ the passive force- length
71 relation, d_m a muscle damping coefficient, and φ the muscle pennation angle.

72 The muscle-tendon parameters consisted of optimum muscle fibre length, l_o^m , tendon
73 slack length, l_s^t , and maximum isometric muscle force, F_o^m , as well as the EMG-to-activation
74 coefficients (C_1 , C_2 and A). These parameters were calibrated for each subject using three
75 strategies: (i) all calibration tasks (ii) sagittal plane calibration tasks, and (iii) scapula plane
76 calibration tasks. In addition, the ‘uncalibrated’ model was also employed where generic values
77 for l_o^m , l_s^t , and F_o^m were taken directly from the scaled musculoskeletal model, and default
78 values of C_1 , C_2 and A were adopted (0.5, -0.5, and 0.1, respectively). Using the four models
79 produced by each calibration strategy, muscle and joint contact forces calculated for abduction
80 and flexion were computed, and joint force compared to published instrumented implant data
81 (Nikooyan et al., 2010, Bergmann et al., 2007). Specifically, data reported by Nikooyan et al.
82 (2010) from two instrumented shoulder implant recipients following hemi-arthroplasty
83 (referred to as ‘implant 1’ and ‘implant 2’, respectively) for the treatment of osteoarthritis
84 without rotator cuff damage (Table 1). The joint replacement procedures were performed using
85 a deltopectoral approach, and joint force data were obtained seven and ten months post-
86 operatively for implant 1 and 2, respectively.

87

88

RESULTS

89 EMG-driven neuromusculoskeletal model calibration strategy had a substantial influence
90 on calculated glenohumeral joint forces for the dynamic shoulder tests (Fig. 1 and Table 2).
91 Calibrating models across all tasks resulted in calculated glenohumeral joint force magnitudes

92 that were more similar to instrumented implant data than those derived from any other model
93 calibration strategy. Specifically, the RMS difference between calculated and measured
94 glenohumeral joint force during abduction was 7.1%BW for implant 1 and 10.8%BW for
95 implant 2 (Table 3).

96 Calibrating the neuromusculoskeletal model using sagittal plane tasks resulted in joint
97 force results that were of similar magnitude to those when the model was calibrated using all
98 tasks. For example, during abduction, the RMS difference between calculated and measured
99 glenohumeral joint force was 8.0%BW and 15.2%BW for implant 1 and 2, respectively. In
100 contrast, calibrating the neuromusculoskeletal model using scapular plane tasks resulted in
101 more substantial differences between calculated and measured glenohumeral joint force, for
102 instance, during abduction the RMS differences between calculated and measured
103 glenohumeral joint force was 13.3%BW and 23.0%BW for implant 1 and 2, respectively. The
104 uncalibrated model resulted in the largest differences between calculated and measured
105 glenohumeral joint force. During abduction, for example, the RMS differences between
106 calculated and measured glenohumeral joint force was 39.9%BW and 55.6%BW for implant 1
107 and 2, respectively.”

108 The middle deltoid, pectoralis major and latissimus dorsi had notably higher muscle
109 forces calculated using the uncalibrated model during abduction (Fig. 2) and flexion (Fig. 3)
110 compared to those calculated using the calibrated models. For these muscles, calibrating the
111 model across all tasks or tasks in one given plane produced similar overall muscle force trends.
112 A neuromusculoskeletal model calibrated across all tasks tended to produce lower muscle
113 forces than that calibrated in the scapular or sagittal plane or when an uncalibrated model was
114 employed.

DISCUSSION

115

116 The present study showed that calibrating EMG-driven neuromusculoskeletal models
117 across a broad range of tasks in multiple planes produced glenohumeral joint forces that were
118 more similar to those measured in instrumented implants than when the models were calibrated
119 only in one plane, or not calibrated at all. Even glenohumeral joint forces computed during
120 abduction using a model calibrated exclusively with tasks in this elevation plane exhibited
121 greater discrepancy with instrumented implant data. The results also demonstrate that net joint
122 moments calculated from neuromusculoskeletal models calibrated across a broad range of tasks
123 were more similar to joint moments calculated from inverse dynamics than when the models
124 were calibrated in one plane or not calibrated at all (see Table 4). These findings suggest that
125 neuromusculoskeletal models that are more extensively calibrated across broad and contrasting
126 tasks produced more physiologically plausible and broadly applicable musculotendon and
127 EMG-to-activation model parameters, and therefore, the most accurate the estimates of muscle
128 and joint loading.

129 When considering data for individual subjects, the results show that model calibration in
130 one plane may in some cases be inadequate and lead to net joint moments and joint forces that
131 are less accurate those than in the case of the uncalibrated model (see Supplementary Material).
132 For example, the RMS difference between the net abduction joint moment and the
133 corresponding inverse dynamics joint moment for subject 1 was 0.22%BWm, 0.86%BWm,
134 1.15%BWm and 0.60%BWm when the model was calibrated using all tasks, calibrated using
135 sagittal plane tasks, calibrated using scapular plane tasks, and not calibrated, respectively. This
136 finding further reinforces the importance of rigorous model calibration across diverse tasks in
137 contrasting motion planes.

138 EMG-driven neuromusculoskeletal model calibration, compared to no calibration, had a
139 substantial impact on the force estimates of prime mover muscles, which included the middle
140 deltoid, pectoralis major and latissimus dorsi, though the force estimates of these muscles were
141 not discernibly different between calibration methods. For a number of other muscles such as
142 the anterior deltoid, posterior deltoid, supraspinatus and subscapularis, calibration method
143 substantially affected calculated muscle forces during abduction and flexion, reflecting greater
144 sensitivity of muscle activation to calibration task. These findings largely reflect the changes
145 in parameters that occurred during model calibration. The calibration algorithm, for instance,
146 was tuned to have greater weighting on a muscle's maximum isometric force, F_o^m , than tendon
147 slack length, l_s^t , which has been shown to have proportionally less variance in healthy cohorts
148 (Wu et al., 2016).

149 This study has some limitations. First, model calibration was primarily across the
150 glenohumeral joint, and different results may occur if the calibration trials explicitly
151 incorporated the elbow, or multiple DOF across both joints. There are other forms of EMG-
152 informed neuromusculoskeletal models, and this study examined EMG-driven models in which
153 all muscles in the model had corresponding EMGs. Calibrated EMG-hybrid models, for
154 instance, also incorporate excitations that are estimated for muscles without recorded EMGs.
155 Nevertheless, in such models we would still expect the contrasting calibration tasks across
156 multiple DOF to improve tracking between excitations and EMGs and joint contact force
157 estimates. Finally, our analysis focused on three test subjects, and this study was therefore not
158 powered for statistical analysis. Nonetheless, this study observed strong trends across all
159 subjects that were used to derive the study conclusions, including differences in computed
160 muscle and joint forces with neuromusculoskeletal model calibration strategy. The consistent
161 patterns of within subject differences in model calibration strategy observed suggests the
162 findings may be generalizable to other subject cohorts.

163 In conclusion, this study demonstrated that extensive model calibration over a broad
164 range of contrasting tasks is required to achieve the most physiologically plausible and broadly
165 applicable musculotendon and EMG-to-activation parameters in EMG-driven
166 neuromusculoskeletal modelling. Quality of model calibration affects muscle forces in a task-
167 dependent manner. The findings of this study will assist in development and deployment of
168 EMG-driven and EMG-informed neuromusculoskeletal models in the estimation of muscle and
169 joint loading.

170

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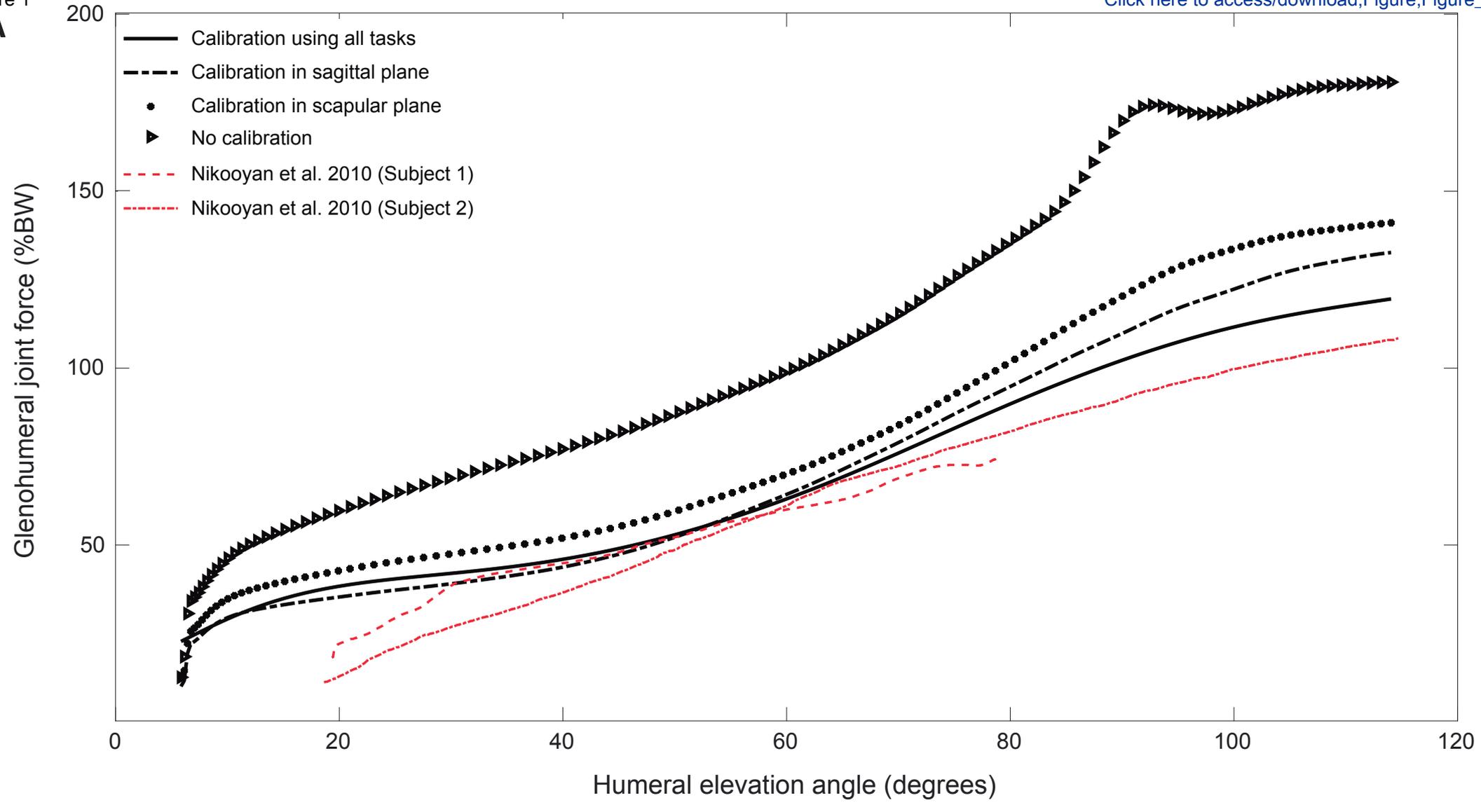
- 174 ASSILA, N., PIZZOLATO, C., MARTINEZ, R., LLOYD, D. G. & BEGON, M. 2020. EMG-
175 Assisted Algorithm to Account for Shoulder Muscles Co-Contraction in Overhead
176 Manual Handling. *Applied Sciences*, 10, 3522.
- 177 BERGMANN, G., GRAICHEN, F., BENDER, A., KÄÄB, M., ROHLMANN, A. &
178 WESTERHOFF, P. 2007. In vivo glenohumeral contact forces—measurements in the
179 first patient 7 months postoperatively. *Journal of Biomechanics*, 40, 2139-2149.
- 180 BOETTCHER, C. E., GINN, K. A. & CATHERS, I. 2008. Standard maximum isometric
181 voluntary contraction tests for normalizing shoulder muscle EMG. *Journal of*
182 *Orthopaedic Research*, 26, 1591-1597.
- 183 GINN, K. A. & HALAKI, M. 2015. Do surface electrode recordings validly represent
184 latissimus dorsi activation patterns during shoulder tasks? *Journal of*
185 *Electromyography and Kinesiology*, 25, 8-13.
- 186 JOHNSON, V. L., HALAKI, M. & GINN, K. A. 2011. The use of surface electrodes to record
187 infraspinatus activity is not valid at low infraspinatus activation levels. *Journal of*
188 *Electromyography and Kinesiology*, 21, 112-118.
- 189 KIAN, A., PIZZOLATO, C., HALAKI, M., GINN, K., LLOYD, D., REED, D. & ACKLAND,
190 D. 2019. Static optimization underestimates antagonist muscle activity at the
191 glenohumeral joint: A musculoskeletal modeling study. *Journal of Biomechanics*, 97,
192 109348.
- 193 LLOYD, D. G. & BESIER, T. F. 2003. An EMG-driven musculoskeletal model to estimate
194 muscle forces and knee joint moments in vivo. *Journal of Biomechanics*, 36, 765-776.
- 195 NIKOOYAN, A., VEEGER, H., WESTERHOFF, P., GRAICHEN, F., BERGMANN, G. &
196 VAN DER HELM, F. 2010. Validation of the Delft Shoulder and Elbow Model using
197 in-vivo glenohumeral joint contact forces. *Journal of Biomechanics*, 43, 3007-3014.
- 198 PIZZOLATO, C., LLOYD, D. G., SARTORI, M., CESERACCIU, E., BESIER, T. F.,
199 FREGLY, B. J. & REGGIANI, M. 2015. CEINMS: A toolbox to investigate the
200 influence of different neural control solutions on the prediction of muscle excitation
201 and joint moments during dynamic motor tasks. *Journal of Biomechanics*, 48, 3929-
202 3936.
- 203 WU, W., LEE, P. V., BRYANT, A. L., GALEA, M. & ACKLAND, D. C. 2016. Subject-
204 specific musculoskeletal modeling in the evaluation of shoulder muscle and joint
205 function. *Journal of Biomechanics*, 49, 3626-3634.

FIGURE CAPTIONS

- Fig. 1. Mean glenohumeral joint force across all subjects (%BW) estimated using the EMG-driven neuromusculoskeletal model for abduction (A) and flexion (B). Shown are results when musculotendon parameters were calibrated using all tasks (solid black line), tasks in the sagittal plane (dash dotted), tasks in the scapular plane (dotted) and in the case of a model with musculotendon parameters that were not calibrated (triangles). *In vivo* glenohumeral joint forces are given for Nikooyan et al., 2010 subject 1 (dashed red line) and subject 2 (dotted red line)
- Fig. 2. Mean muscle forces across all subjects (%BW) estimated using the EMG-driven neuromusculoskeletal model during scapular-plane abduction. Shown are results when musculotendon parameters were calibrated using all tasks (solid line), tasks in the sagittal plane (dash dotted), tasks in the scapular plane (dotted), and in the case of a model with musculotendon parameters that were not calibrated (dashed). Data are given for nine selected muscles spanning the glenohumeral joint including the anterior deltoid (DeltA), middle deltoid (DeltM), posterior deltoid (DeltP), supraspinatus (Supra), infraspinatus (Infra), subscapularis (Subs), pectoralis major (PMaj), latissimus dorsi (LDorsi) and teres major (TMaj).
- Fig. 3. Mean muscle forces across all subjects estimated using the EMG-driven neuromusculoskeletal model during flexion. Given are results when musculotendon parameters were calibrated using all tasks (solid line), tasks in the sagittal plane (dash dotted), tasks in the scapular plane (dotted), and in the case of a model with musculotendon parameters that were not calibrated

(dashed). Data are given for nine selected muscles spanning the glenohumeral joint. For muscle definitions see caption of Figure 2.

A



B

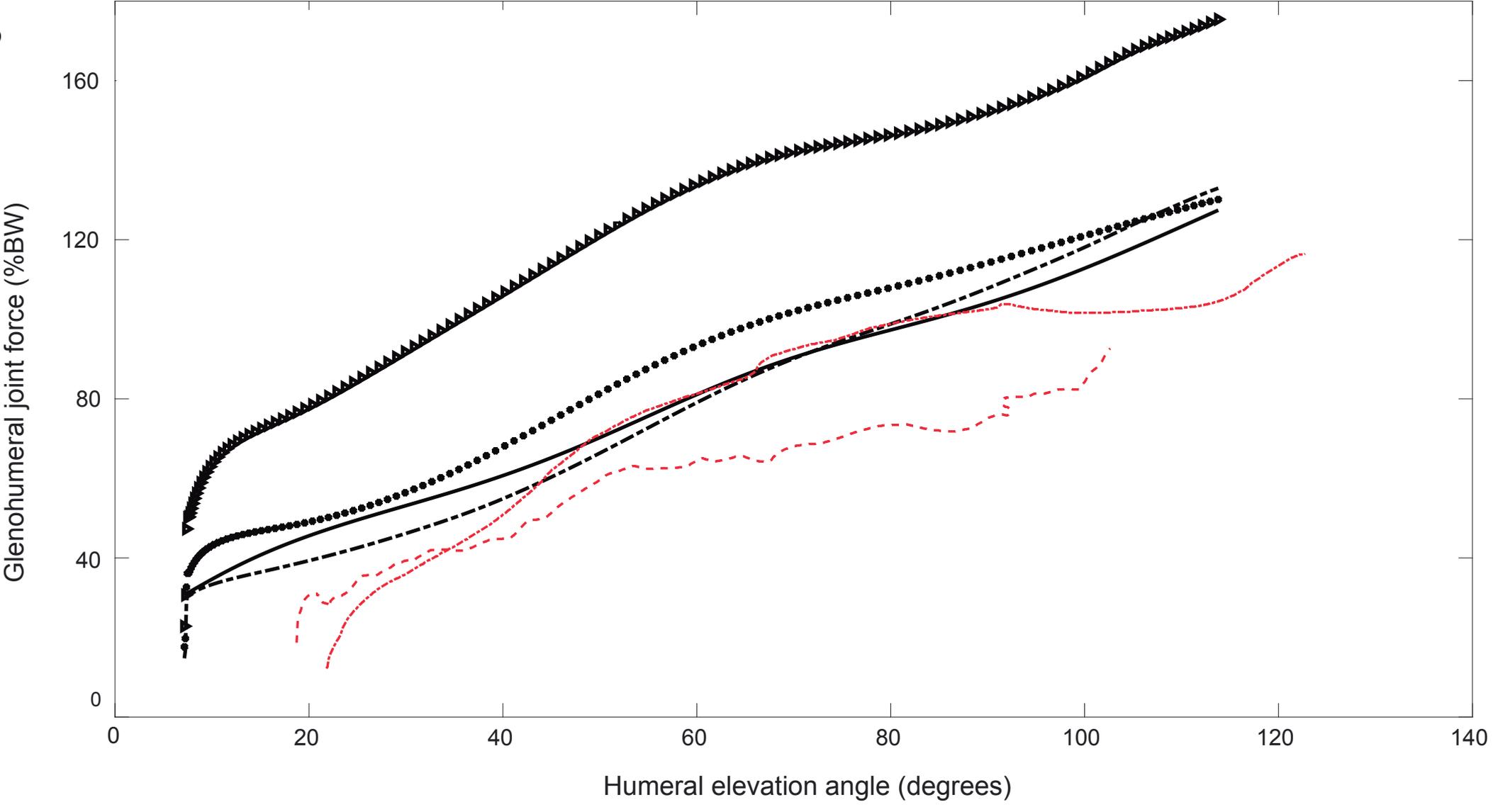
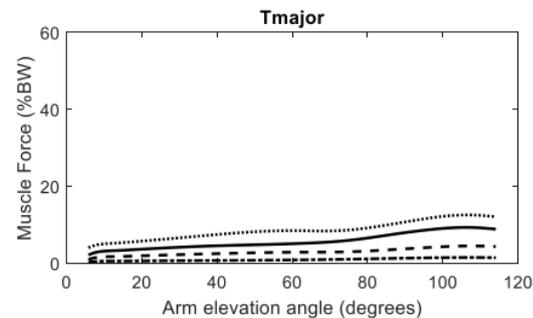
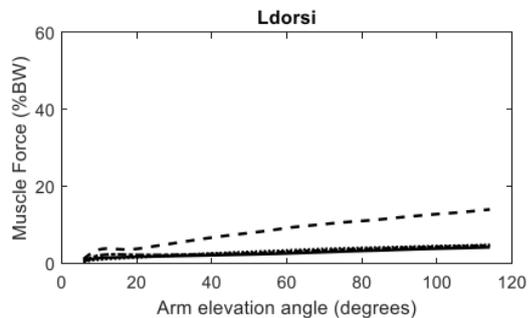
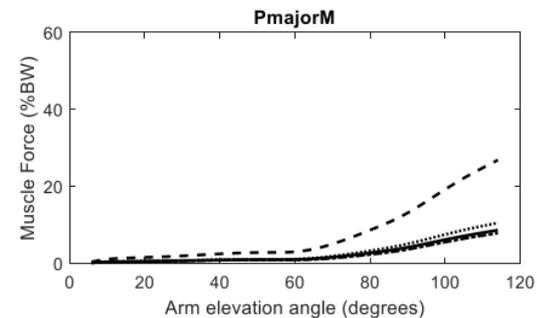
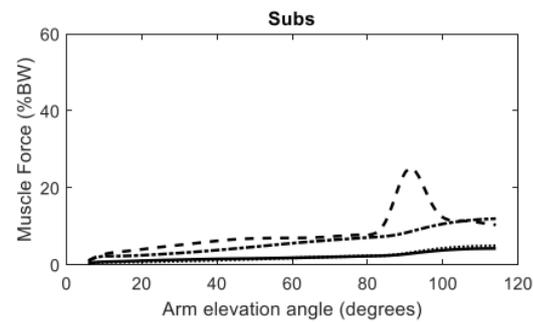
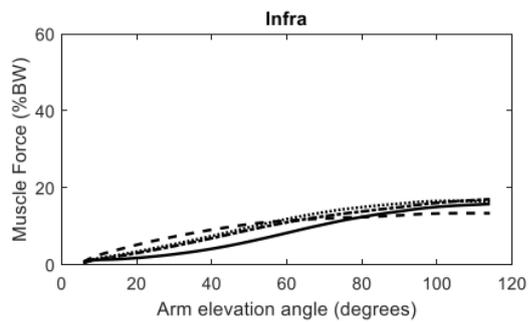
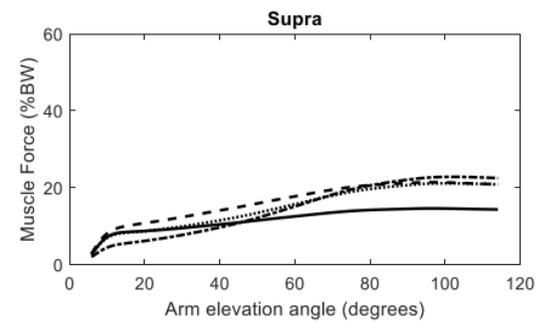
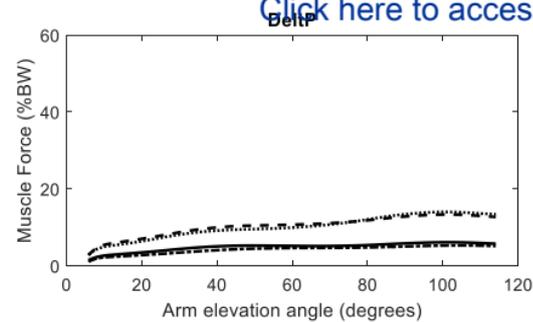
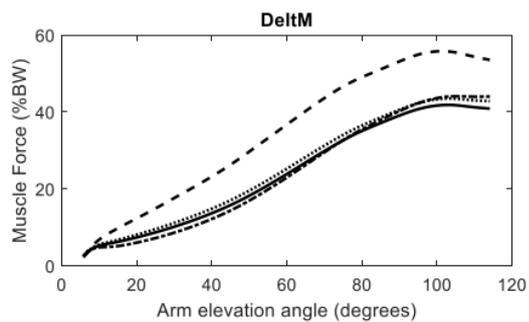
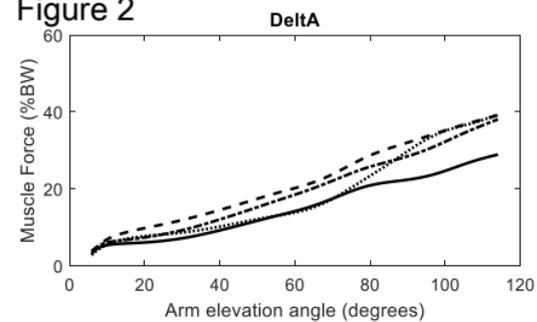
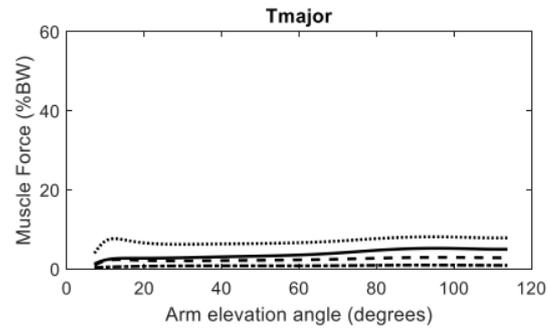
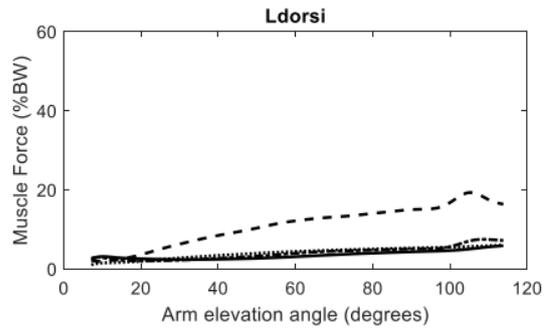
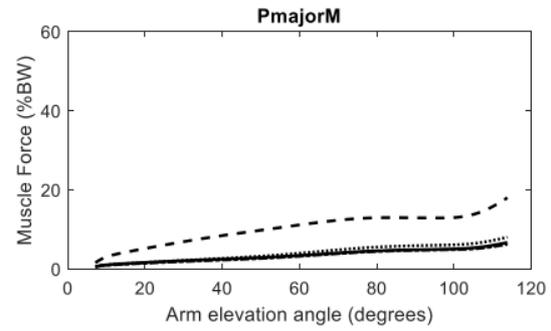
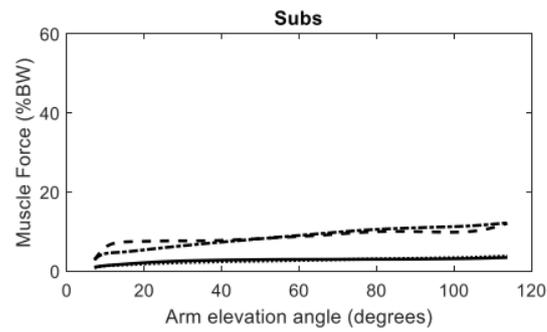
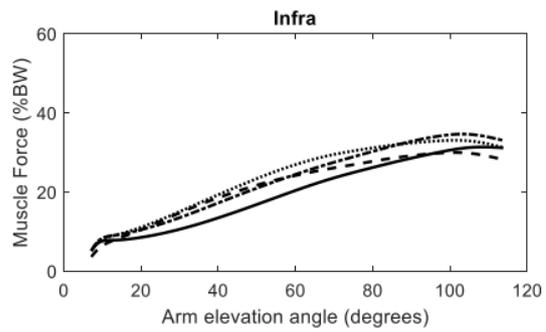
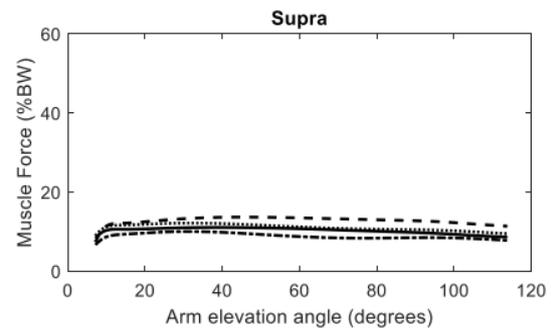
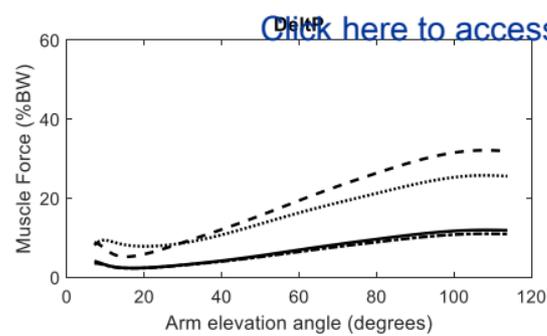
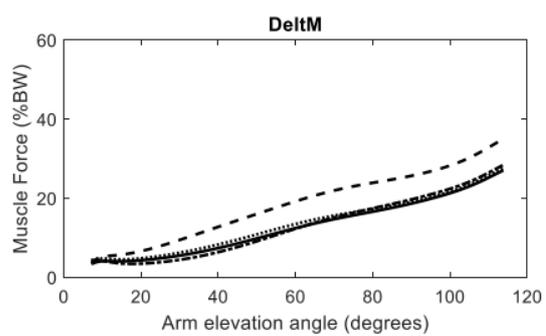
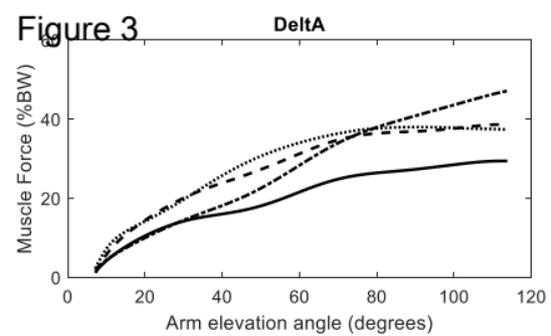


Figure 2



- No calibration
- .- Calibration in sagittal plane
- ... Calibration in scapular plane
- Calibration using all tasks



- No calibration
- - - Calibration in sagittal plane
- ... Calibration in scapular plane
- Calibration using all tasks

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Table 1: Demographic data for participants in the current study. Instrumented implant data previously reported by Nikooyan et al. 2010 are indicated with an asterisk.

	Sex	Age (yrs)	Height (cm)	Weight(kg)	BMI (kg/m²)	Side
Subject 1	Female	31	164	57	21.2	Right
Subject 2	Female	19	168	52	18.4	Right
Subject 3	Female	21	163	58	21.8	Right
Implant 1*	Female	73	168	72	25.5	Left
Implant 2*	Male	64	163	85	32	Right

Table 2: Mean and standard deviation (SD) data for glenohumeral joint force magnitude (%BW) calculated using an EMG-driven neuromusculoskeletal model. Data are provided for the model when calibrated using all tasks, calibrated in the sagittal plane and scapular plane, and when not calibrated. Given are results for shoulder abduction in the scapular plane and flexion in the sagittal plane.

	Abduction						Flexion					
	30 degrees		60 degrees		90 degrees		30 degrees		60 degrees		90 degrees	
	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD
Calibration using all tasks	41.9	4.0	63.7	25.4	102.3	54.4	53.7	11.9	81.7	19.4	104.4	37.0
Calibration in sagittal plane	39.0	7.2	65.0	36.5	109.8	67.3	46.8	6.4	79.8	26.6	108.1	43.0
Calibration in scapular plane	47.4	8.9	70.7	20.3	120.4	61.1	57.3	18.3	94.0	31.8	114.4	45.0
No model calibration	68.8	9.1	99.8	23.1	169.9	29.0	93.2	8.9	134.7	19.9	152.4	24.3

Table 3: RMS differences in glenohumeral joint force magnitude (%BW) estimated between the EMG-driven neuromusculoskeletal model and *in vivo* instrumented implant measurements reported by Nikooyan et al., (2010) for two subjects, denoted implant 1 and implant 2. Data are provided for the model when calibrated using all tasks, calibrated in the sagittal plane and scapular plane, and when not calibrated. Given are results for shoulder abduction in the scapular plane and flexion in the sagittal plane.

	Abduction		Flexion	
	Implant 1	Implant 2	Implant 1	Implant 2
Calibration using all tasks	7.1	10.8	20.4	11.7
Calibration in sagittal plane	8.0	15.2	20.8	12.0
Calibration in scapular plane	13.2	23.0	28.8	16.9
No model calibration	39.9	55.6	67.1	55.4

Table 4: RMS differences in net glenohumeral joint moments (%BW.m) between the EMG-driven neuromusculoskeletal model calculations and those computed directly using inverse dynamics. Data are provided for the model when calibrated using all tasks, calibrated in the sagittal plane and scapular plane, and when not calibrated. Given are results for shoulder abduction in the scapular plane and flexion in the sagittal plane.

	<u>Abduction</u>	<u>Flexion</u>
Calibration using all tasks	0.14	0.09
Calibration in sagittal plane	0.17	0.16
Calibration in scapular plane	0.20	0.17
No model calibration	0.47	0.28



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